

City of Coos Bay

STRUCTURAL CALCULATIONS

Mingus Pool Building Coos Bay
Coos Bay, Oregon

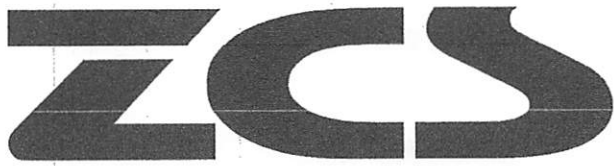
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REVIEWED BY: Syllas E. Allen, PE



EXPIRES: 12-31-17

4/6/16
Job Number: G-0703-14



ENGINEERING inc

CLIENT City of Coos Bay

PROJECT Mingus Pool

Retaining Wall Design

NO. G-703-14

BY KMH DATE _____ SHEET _____ OF _____

Grants Pass • Klamath Falls • Medford • Oregon City

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Lateral Pressures on Wall

Active Earth Pressure :

$$P_a = \frac{1}{2} (.26)(5')^2 (115 \text{ pcf}) = 375 \text{ p1F}$$

$$\phi = 36^\circ$$

$$\delta = 115 \text{ pcf}$$

$$k_a = \frac{1 - \sin 36}{1 + \sin 36} = .26$$

Surcharge :

1. Slab = Live

$$\text{Slab} = (160 \text{ pcf}) \left(\frac{6''}{12}\right) = 80 \text{ psf}$$

$$\text{Live} = 125 \text{ psf}$$

$$\text{Total} = 205 \text{ psf}$$

$$P_q = (205)(.26)(5') = 267 \text{ p1F}$$

$$P_{\text{Total}} = 642 \text{ p1F}$$

Concrete Beam

\\Oc001\gpi\2014\IG-0703-14_City of Coos Bay\Mingus Pool Building Coos Bay\Structural\Calculations\tank wall.ec6
 ENERCALC, INC. 1983-2016, Build:6.16.2.18, Ver:6.16.2.18

Lic. #: KW-06004512

Licensee: ZBINDEN-CARTER ENGINEERING

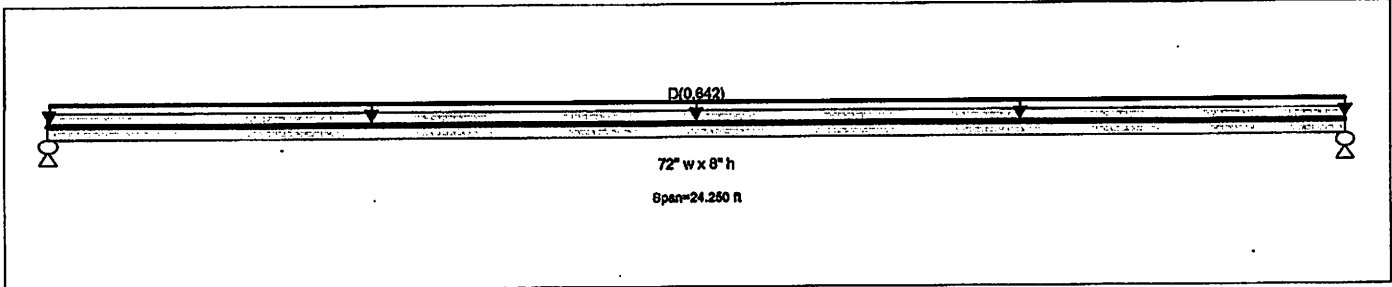
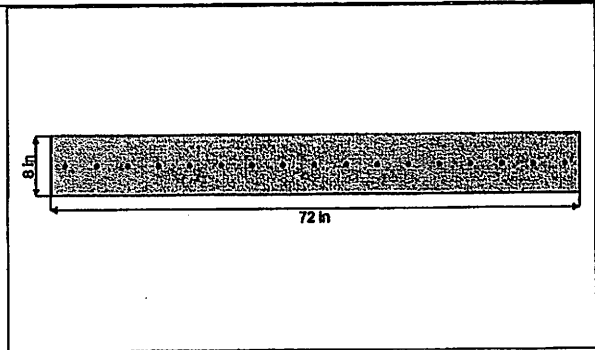
Description: Tank Wall (KMH)

CODE REFERENCES

Calculations per ACI 318-11, IBC 2012, ASCE 7-10
 Load Combination Set: ASCE 7-05

Material Properties

f_c	=	4.50 ksi	ϕ Phi Values	Flexure:	0.90
$f_r = f_c^{1/2} * 7.50$	=	503.12 psi		Shear:	0.750
Ψ Density	=	145.0 pcf	β_1	=	0.8250
λ LWt Factor	=	1.0			
Elastic Modulus	=	3,122.0 ksi	Fy - Stirrups	=	40.0 ksi
fy - Main Rebar	=	60.0 ksi	E - Stirrups	=	29,000.0 ksi
E - Main Rebar	=	29,000.0 ksi	Stirrup Bar Size #	=	3
			Number of Resisting Legs Per Stirrup	=	2



Cross Section & Reinforcing Details

Rectangular Section, Width = 72.0 in, Height = 8.0 in
 Span #1 Reinforcing....
 17-#5 at 4.0 in from Top, from 0.0 to 24.250 ft in this span

Applied Loads

Service loads entered. Load Factors will be applied for calculations.

Load for Span Number 1

Uniform Load: D = 0.6420 k/ft, Tributary Width = 1.0 ft

DESIGN SUMMARY

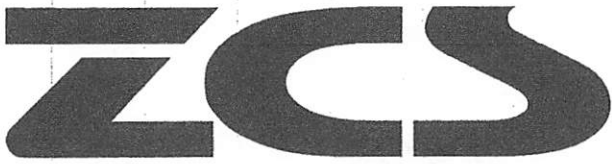
Design OK

Maximum Bending Stress Ratio =	0.813 : 1	Maximum Deflection		
Section used for this span	Typical Section	Max Downward Transient Deflection	0.000 in	Ratio = 0 < 360
Mu : Applied	86.069 k-ft	Max Upward Transient Deflection	0.000 in	Ratio = 0 < 360
Mn * Phi : Allowable	81.246 k-ft	Max Downward Total Deflection	1.270 in	Ratio = 229 >= 18
		Max Upward Total Deflection	0.000 in	Ratio = 999 < 180
Location of maximum on span	12.147 ft			
Span # where maximum occurs	Span # 1			

Vertical Reactions

Support notation: Far left is #1

Load Combination	Support 1	Support 2
Overall MAXimum	7.784	7.784
Overall MINimum	4.671	4.671
D Only	7.784	7.784
+D+L	7.784	7.784
+D+Lr	7.784	7.784
+D+S	7.784	7.784
+D+0.750Lr+0.750L	7.784	7.784
+D+0.750Lr+0.750S	7.784	7.784
+D+W	7.784	7.784
+D+0.70E	7.784	7.784
+D+0.750Lr+0.750L+0.750W	7.784	7.784
+D+0.750Lr+0.750S+0.750W	7.784	7.784
+D+0.750Lr+0.750L+0.5250E	7.784	7.784
+D+0.750Lr+0.750S+0.5250E	7.784	7.784



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Conduit Support

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DL

◦ Schedule 80 6" PVC Pipe DL = 6 p/f

$$\text{weight of water} = (62.4 \text{ pcf}) \left(\frac{\pi}{4} \right) (6/12)^2 = 13 \text{ p/f}$$

$$\text{Total} = 19 \text{ p/f} \Rightarrow \text{Use } 20 \text{ p/f} \text{ for support structure}$$

max of (3) 6" ϕ PVC pipes ◦ Design for (3.5) Pipes to be conserv.

Use

$$(3)(20 \text{ p/f}) = 60 \text{ p/f} \text{ for design load of support structure}$$

Conduit Span Check

$$S_{\text{pipe}} = \frac{\pi(d^4 - d_i^4)}{32d} = \frac{\pi(6.625^4 - 5.761^4)}{32(6.625)} = 12.2 \text{ in}^3$$

$$M_{\text{max}} = \frac{(0.019)(19' \times 12)^2}{8} = 27.8 \text{ k-in}$$

$$I = \frac{\pi(6.625^4 - 5.761^4)}{64}$$

$$I = 40.5 \text{ in}^4$$

$$f_b = \frac{27.8 \text{ k-in}}{12.2 \text{ in}^3} = 2.03 \text{ ksi} < 7.2 \text{ ksi} \text{ } \checkmark \text{ok Bending}$$

$$\Delta_{\text{max}} = \frac{5wl^4}{384EI} = \frac{5(0.019 \text{ k/f})(19')(19 \times 12)^3}{384(430 \text{ ksi})(40.5 \text{ in}^4)} = 0.17 \text{ in} < 0.3 \text{ } \checkmark \text{ok}$$

$$\Delta_{\text{allow}} = \frac{(a)(12)}{360} = 0.3 \text{ in}$$